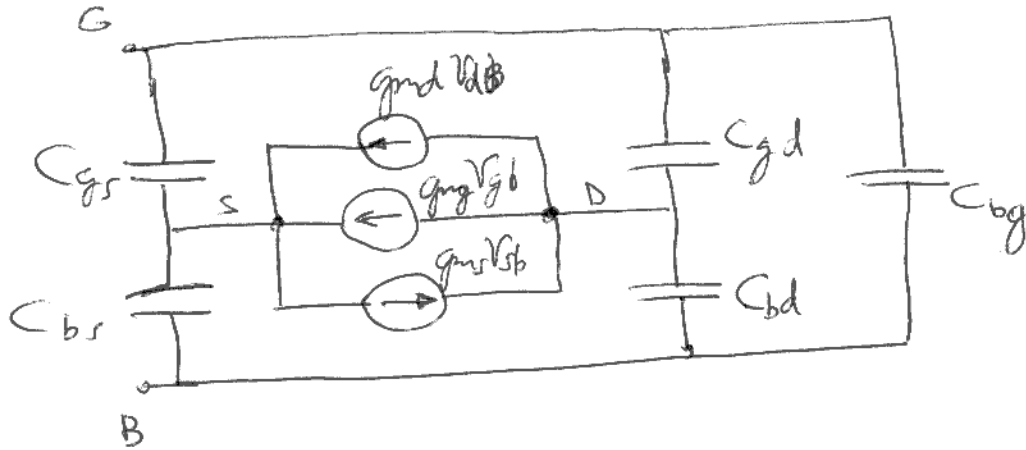


# MOSFET CAPACITANCES

①

## QUASI-STATIC MODEL



• MODEL VALID IF  $\omega \tau_i \ll 1$

$$\tau_i \approx \begin{cases} \frac{4}{15} \frac{\tau}{\beta} & \text{ACTIVE REGION, STRONG INVERSION} \end{cases}$$

$$\begin{cases} \frac{\tau}{6} & \text{WEAK INVERSION (ANY REGION)} \end{cases}$$

$$\tau = \frac{L^2}{\mu V_T}$$

$$\alpha = \frac{\sqrt{1+\beta} - 1}{\sqrt{1+\beta}}$$

$$C_{gs} = \frac{2}{3} C'_{ox} \frac{1+2\alpha}{(1+\alpha)^2} \frac{\sqrt{1+\beta} - 1}{\sqrt{1+\beta}}$$

$$C_{gd} = \frac{2}{3} C'_{ox} \frac{\alpha^2 + 2\alpha}{(1+\alpha)^2} \frac{\sqrt{1+\beta} - 1}{\sqrt{1+\beta}}$$

$$C_{bg} = \frac{n-1}{n} (C'_{ox} - C_{gs} - C_{gd})$$

$$C_{bs} = (n-1) C_{gs}, \quad C_{bd} = (n-1) C_{gd}$$

$C'_{ox}$  HERE IS  
 $\frac{C_{ox} \times W \times L}{\text{TOTAL GATE CAPACITANCE}}$

1) STRONG INVERSIONTRIODE, ASSUME  $i_f = i_r \Rightarrow \alpha = 1$ 

$$C_{gs} \approx \frac{1}{2} C_{ox}$$

$$C_{gd} \approx \frac{1}{2} C_{ox}$$

$$C_{gb} \approx 0 \quad (\text{MASKED BY CHANNEL})$$

ACTIVE  $\Rightarrow \alpha \approx 0$ 

$$C_{gs} = \frac{2}{3} C_{ox}$$

$$C_{gd} \approx 0$$

$$C_{bg} \approx \left(\frac{n-1}{n}\right) \frac{C_{ox}}{3}$$

2) WEAK INVERSIONTRIODE,  $i_f = i_r \Rightarrow \alpha = 1$ 

$$C_{gs} \approx \frac{1}{4} C_{ox} i_f \quad \left. \begin{array}{l} \text{NOTICE } i_f, i_r \text{ SMALL,} \\ \text{SO CAPACITANCES ALSO SMALL} \end{array} \right\}$$

$$C_{gd} \approx \frac{1}{4} C_{ox} i_r$$

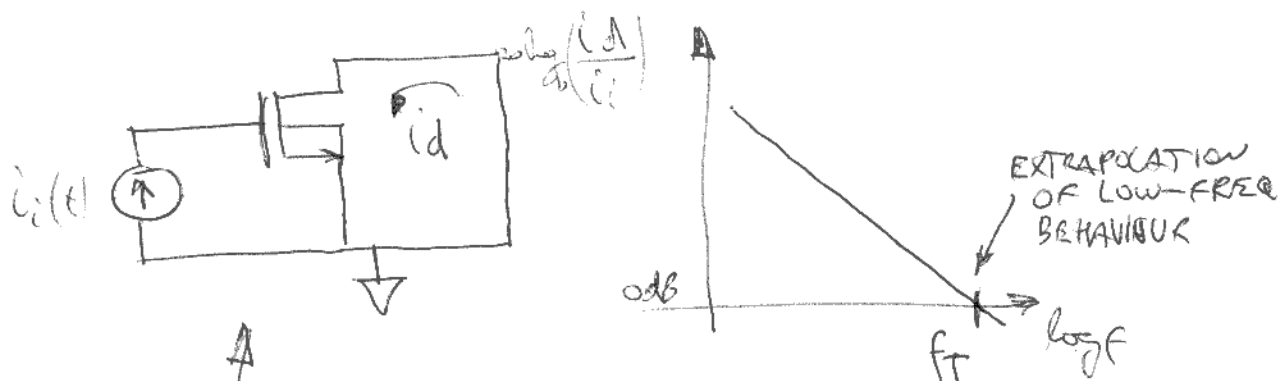
$$C_{bg} \approx \frac{n-1}{n} C_{ox} \quad \leftarrow \text{MOST OF GATE CAPACITANCE GOES TO BULK}$$

ACTIVE,  $\alpha \approx 1 \Rightarrow$  SAME AS TRIODE

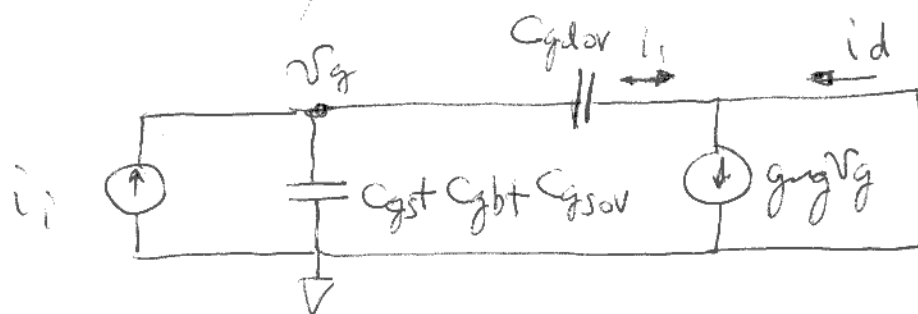
NOTE: THIS CAPACITANCES ONLY VALID FOR SMALL-SIGNAL MODEL. FOR LARGE-SIGNAL, NONLINEAR CHARGES MUST BE USED.

# TRANSITION FREQUENCY ( $f_T$ )

(3)



(SMALL SIGNAL)



NOTE: FOR ACTIVE MODE  $C_{gd}$  NEGLIGIBLE COMPARED TO  $C_{gdov}$

ASSUMPTION: @ LOW FREQUENCIES  $i_i \ll i_d$

$$\therefore i_d \approx g_m v_g$$

$$v_g = i_i \times X_{C_T}, \quad C_T = C_{gs} + C_{gb} + C_{gout} + C_{gdov}$$

$$v_g = \frac{i_i}{j\omega C_T}$$

$$\left| \frac{i_d}{i_i} \right| = \frac{g_m}{\omega C_T} = 1 \quad \left( \omega = \omega_T \right)$$

$$f_T = \frac{g_m}{2\pi C_T}$$

$$f_T = \frac{2 I_s}{n V_T \times 2\pi C_T} (\sqrt{1+ic} - 1) = \frac{\mu C_{ox} \left(\frac{W}{L}\right) V_T}{2\pi C_T} (\sqrt{1+ic} - 1) \quad (4)$$

$$I_s = \frac{n \mu C_{ox} V_T^2 \left(\frac{W}{L}\right)}{2}$$

OBSERVATION: ASSUMING  $C_T$  DOES NOT CHANGE MUCH,  
STRONGER INVERSION ACHIEVES HIGHER  $f_T$

- CONSIDER NOW ONLY THE INTRINSIC CAPACITANCES,  
AND APPROXIMATE  $C_{gs} + C_{gb} \approx \frac{1}{2} C_{ox} WL$  (AVERAGE FOR WEAK-STRONG INVERSION)

$$(*) \quad f_T \approx \frac{\mu C_{ox} \frac{W}{L} V_T}{2\pi \times \frac{1}{2} C_{ox} WL} (\sqrt{1+ic} - 1) = \frac{\mu C_{ox} V_T}{\pi C_{ox} L^2} (\sqrt{1+ic} - 1)$$

OBSERVATION: SHORTER CHANNEL  $\Rightarrow f_T \uparrow$

RULE OF THUMB: TRANSISTOR USEFUL FOR AMPLIFICATION UP TO  $\left(\frac{f_T}{10}\right)$ .

(\*) CONSIDERING OVERLAP CAPACITANCES:

$$f_T \approx \frac{\mu V_T}{2\pi \left[\frac{L^2}{2} + 2L\Delta L\right]} (\sqrt{1+ic} - 1)$$