

1) EXTRACTED PARAMETERS FOR  $\frac{W}{L} = \frac{10\mu\text{m}}{10\mu\text{m}}$

$$\left. \frac{g_m}{I_D} \right|_{\text{PEAK}} \approx 25.6$$

$$\boxed{V_{th} = V_G @ 53\% \left. \frac{g_m}{I_D} \right|_{\text{PEAK}} = 746 \text{ mV}}$$

$$I_S = (I_D @ V_{th}) \times 1.13 = \boxed{116 \text{ nA} = I_{SQ}}$$

(NEGLECTING  $L_D$  SINCE  $L \gg L_D$ )

$$\left. \begin{aligned} n \Big|_{V_S=0} &= 1.47 \\ V_G &= V_{th} \end{aligned} \right\}$$

→ WILL USE  $n \approx 1.4$  FOR MANUAL CALCULATIONS

• OUTPUT RESISTANCE: USING  $V_G = V_{th}$

$$\left. \begin{aligned} \Delta V_{DS} &= 2\text{V} - 0.5\text{V} \\ \Delta I_D &= 386 \text{ nA} - 379 \text{ nA} \end{aligned} \right\} \frac{\Delta V_{DS}}{\Delta I_D} = 214 \text{ M}\Omega = r_o$$

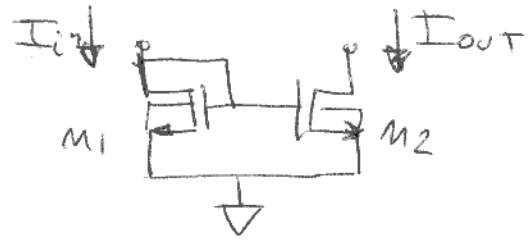
$$V_A \approx r_o \times I_D = 81 \text{ V} = \frac{L}{\left| \frac{\partial X_D}{\partial V_{DS}} \right|}$$

$$\therefore \left| \frac{\partial X_D}{\partial V_{DS}} \right| = \boxed{0.123 \frac{\mu\text{m}}{\text{V}}}$$

2)

2)  $W = 30 \mu\text{m}$   
 $L = 2 \mu\text{m}$   
 $V_{DD} = 2\text{V}$

$I_{in} = \begin{cases} 10 \mu\text{A} \\ 5 \mu\text{A} \\ 100 \mu\text{A} \end{cases}$



a)  $V_{S1} = V_{S2} = 0$

$\frac{V_G - V_{th}}{n V_T} = \mathcal{F}(i_f) \quad I_S = 116 \text{ nA} \times \frac{30 \mu\text{m}}{(2 \mu\text{m} - 2 \times 20 \text{ nm})} = 1.78 \mu\text{A}$

$i_f = ? \quad I_{in} = I_{sa} \frac{W}{L_{eff}} i_{f1}$

$i_{f1} = \begin{cases} 0.00563 \\ 2.81 \\ 56.3 \end{cases} \rightarrow \mathcal{F}(i_{f1}) = \begin{cases} -6.87 \\ -0.097 \\ 7.45 \end{cases}$

$\therefore V_{G1} = V_{D1} = \begin{cases} 0.498 \text{ V} \\ 0.742 \text{ V} \\ 1.02 \text{ V} \end{cases}$   
 $V_{th} + n V_T \mathcal{F}(i_{f1})$

b)  $R = \frac{V_{DD} - V_{G1}}{I_{in}} = \begin{cases} 150.4 \text{ M}\Omega \\ 252 \text{ k}\Omega \\ 9.8 \text{ k}\Omega \end{cases}$

c)  $V_{DSAT_2} = V_T (\sqrt{1+i_{f_2}} + 3)$

$$V_{OUT\ min} = \begin{cases} 104\ \text{mV} \\ 129\ \text{mV} \\ 275\ \text{mV} \end{cases}$$

d)  $\Delta I$  DUE TO DIFFERENCE IN  $V_{DS_1}$  AND  $V_{DS_2}$

$$\left. \begin{array}{l} V_{DS_1} = V_{G1} \\ V_{DS_2} = 2V \end{array} \right\} \Rightarrow \Delta I_{1-2} = \frac{2V - V_{G1}}{r_o} = \left( \frac{2V - V_{G1}}{V_A} \right) I_D$$

$$V_A = \frac{L}{\left| \frac{\partial x_D}{\partial V_{DS}} \right|} = 15.9\ \text{V}$$

$$\Delta I_{1-2} = \begin{cases} 0.94\ \text{mA} \\ 0.396\ \mu\text{A} \\ 6.16\ \mu\text{A} \end{cases}$$

e)  $V_G - V_{th} = n V_T \Phi(i_f)$

$$V_{th} = V_G - n V_T \Phi(i_f)$$

$$V_{th} + \Delta V_{th} = V_G - n V_T \Phi(i_f) \approx n V_T \frac{d\Phi(i_f)}{d i_f} \Delta i_f$$

$$\Delta V_{th} = -n V_T \frac{d\Phi(i_f)}{d i_f} \Delta i_f$$

$$|\Delta i_f| = \frac{\Delta V_{th}}{n V_T \frac{d\Phi(i_f)}{d i_f}} = \frac{\Delta V_{th}}{n V_T} \times 2 (\sqrt{1+i_f} - 1)$$

• ANOTHER APPROACH: RECOGNIZING THAT  $V_{th}$  AND  $V_G$  HAVE SAME EFFECT ON  $i_f$  (WITH OPPOSITE SIGN)

④  ~~$\Delta I_D$~~   $|\Delta I_D| = |i_d| = g_m g_m \Delta V_{th} \approx \frac{g_m I_S}{n} \Delta V_{th}$   
ACTIVE

$|\Delta I_D| = \frac{2 I_S}{n V_T} (V_{th}^{i_f} - 1) = \Delta i_f \times I_S$   
 (SAME RESULT AS BEFORE)

$\Delta I_D = \begin{cases} 2.75 \text{ nA} \\ 0.93 \text{ } \mu\text{A} \\ 6.43 \text{ } \mu\text{A} \end{cases}$	$\frac{\Delta I_D}{I_D} = \begin{cases} 27.4\% \\ 18.6\% \\ 6.4\% \end{cases}$
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3)

	PARAMETER	CALCULATED	SIMULATED
10 nA	$V_{en} \text{ (mV)}$	496	480.7
	$V_{o, min} \text{ (mV)}$	104	41.32 (*)
	$\Delta I \text{ (nA)}$	0.94	0.5

5  $\mu\text{A}$

$V_{in} \text{ (mV)}$	742	767
$V_{o, min} \text{ (mV)}$	129	72.7 (*)
$\Delta I \text{ (nA)}$	930	124

100  $\mu\text{A}$

$V_{in} \text{ (mV)}$	1020	1022
$V_{o, min} \text{ (mV)}$	275	237 (*)
$\Delta I \text{ (nA)}$	6430	800

COMMENTS = •  $V_{in}$  AGREEMENT IS GOOD

(5)

(\*) •  $V_{o, min}$  WAS ESTIMATED IN SIMULATIONS USING THE VALUE OF  $V_{D, SAT}$   
RESULTS → PRINT → DC OPERATING POINTS

MANUAL CALCULATION IS BETTER

(SEE GRAPH)

(RAZAVI RECOMMENDS: FOR SIMULATIONS)  
(LOOK AT GRAPHS, NOT JUST VALUES.)

•  $\Delta I$  IN CALCULATIONS IS MORE PESSIMISTIC THAN IN SIMULATIONS. AGREEMENT DEPENDS ON EXTRACTED VALUE OF  $\left| \frac{\partial X_D}{\partial V_{DS}} \right|$ . IN GENERAL, A PESSIMISTIC VALUE IS SAFER THAN AN OPTIMISTIC ONE.